

Fractional and irrational differential systems: approximation and optimization

T. HÉLIE

Collaboration with D.Matignon and R. Mignot

— Fractional Derivatives for Mechanical Engineering - State-of-the-art and Applications —

- 1 **Introduction : zoology and basic ideas**
- 2 **Systems under consideration**
 - Integral representations with poles and cuts
 - Finite-dimensional approximation by interpolation
- 3 **Specialized optimization procedures**
 - Functional spaces and measures
 - Regularized criterion with equality constraints
 - Numerical optimization
- 4 **Applications**
 - Fractional systems
 - Irrational systems
- 5 **Conclusion and Perspectives**

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Zoology of $\underline{e(t)}$ Fractional/Irrational Syst. $\underline{y(t)}$

Fractional/Irrational syst.	Transfer fct. (analytic in $\Re(s) > 0$)
Integrator $I_{1/2}$	$H_1(s) = 1/\sqrt{s}$ ($\rightarrow H(s)^2 = 1/s$)
Derivative $\partial_t^{1/2}$	$H_2(s) = \sqrt{s}$ ($\rightarrow H(s)^2 = s$)
Frac. Diff. Eq. ($0 < \alpha < 1$) $\sum_{p=0}^P \partial_t^{p\alpha} y = \sum_{q=0}^Q \partial_t^{q\alpha} e$	$H_3(s) = \sum_{q=0}^Q s^{q\alpha} / \sum_{p=0}^P s^{p\alpha}$

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Bessel : $y(t) = [J_0 \star u](t)$	$H_4(s) = 1/\sqrt{s^2 + 1}$
Fract. PDE : $(\partial_z + \partial_t^{1/2})x = 0$ $y(t) = x(z, t), \partial_z x(0, t) = -e(t)$	$H_5(s) = e^{-\sqrt{s}z} / \sqrt{s}$
Flared lossy acoustic pipe	$H_6(s) = 2\Gamma(s)e^{s-\Gamma(s)} / [s + \Gamma(s)]$ with $\Gamma(s) = \sqrt{s^2 + \varepsilon s^{3/2} + 1}$

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\rightarrow **singularities of $H_k(s)$** : poles and **cuts** in $\Re e(s) < 0$

Case of the fractional integrator $I_{1/2}$ ($H_1(s) = 1/\sqrt{s}$)

- Consider $s = \rho e^{i\theta} \in \mathbb{C}$ with $\rho > 0$ and $\theta \in]-\pi, \pi]$

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\mathbb{R}^- is called a **cut** of $H_1(s)$ and the **jump** at $-\xi \in \mathbb{R}^-$ is

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- Why choosing the cut \mathbb{R}^- (that is $\theta \in] - \pi, \pi]$) ?**
 - Causal stable system $\Rightarrow H$ analytic in $\Re(s) > 0$
 - It is “natural” to preserve the Hermitian symmetry since a real system $\Rightarrow H_1(\bar{s}) = \overline{H_1(s)}$ in $\Re(s) > 0$

Basic idea : adapted Bromwich contour

Let $e_+^t = e^t \mathbf{1}_{\mathbb{R}^+}(t)$ be the causal exponential.

- Causal convolution kernel : $h_1(t) = \lim_{\epsilon \rightarrow 0^+} \int_{\epsilon - i\infty}^{\epsilon + i\infty} H_1(s) e_+^{st} ds$

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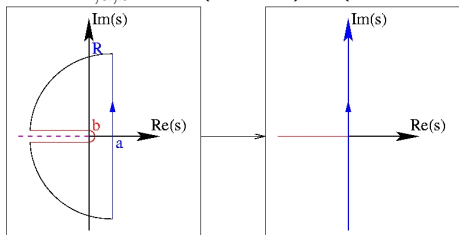
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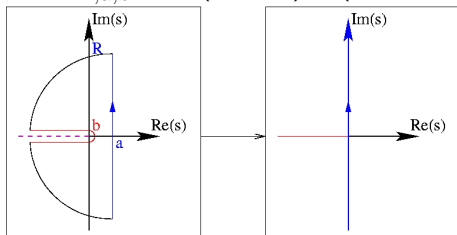
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- $h(t) + 0 - \int_0^{+\infty} \mu(-\xi) e_+^{-\xi t} d\xi + 0 = 0$ with $\mu(-\xi) = \frac{H_1(-\xi + i0^-) - H_1(-\xi + i0^+)}{2i\pi} = \frac{1}{\pi\sqrt{\xi}}$

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$$\begin{cases} \partial_t \phi(-\xi, t) = -\xi \phi(-\xi, t) + e(t), & \phi(-\xi, 0) = 0, \quad \forall \xi > 0 \\ y(t) = \int_0^{+\infty} \mu(-\xi) \phi(-\xi, t) d\xi \end{cases}$$

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- Transfer function : **aggregation of first order systems**

$$F(-\xi, s) = \frac{\Phi(-\xi, s)}{E(s)} = \frac{1}{s + \xi}, \quad \forall \xi > 0$$

$$\begin{aligned} H_1(s) &= \frac{Y(s)}{E(s)} = \frac{\int_0^{+\infty} \mu(-\xi) \Phi(-\xi, s) d\xi}{E(s)} = \int_0^{+\infty} \mu(-\xi) F(-\xi, s) d\xi \\ &= \int_0^{+\infty} \frac{\mu(-\xi)}{s + \xi} d\xi \quad \left(= \frac{1}{\sqrt{s}} \right), \quad \text{for } \Re e(s) > 0 \end{aligned}$$

Basic idea : generalizations and questions

Summary :

- Determine the **singularities (poles and cuts)** of $H(s)$.

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- Are such integral representations always **well-posed** ?
- How to perform accurate **approximations and simulations in the time domain** ?

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Definitions

- Many **transfer functions** can be decomposed as follows, in some right-half complex plane $\mathbb{C}_a^+ := \{\Re e(s) > a\}$,

$$H(s) = \sum_{k=1}^K \sum_{l=1}^{L_k} \frac{r_{k,l}}{(s - s_k)^l} + \int_{\mathcal{C}} \frac{M(d\gamma)}{s - \gamma},$$

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- which translates in the time domain into the following decomposition of the **impulse response** :

$$h(t) = \sum_{k=1}^K \sum_{l=1}^{L_k} r_{k,l} \frac{1}{l!} t^{l-1} e^{s_k t} + \int_{\mathcal{C}} e^{\gamma t} M(d\gamma), \quad \text{for } t > 0.$$

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- The **integral part** can be realized by a **dynamical system** :

$$\partial_t \phi(\gamma, t) = \gamma \phi(\gamma, t) + u(t), \quad \phi(\gamma, 0) = 0, \quad \forall \gamma \in \mathcal{C}$$

$$y(t) = \int_{\mathcal{C}} \phi(\gamma, t) M(d\gamma),$$

Some technical conditions

- A **well-posedness** condition must be fulfilled :

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- Note the **hermitian symmetry** property :

$$H(s) = \overline{H(\bar{s})}, \forall s \in \mathbb{C}_a^+$$

Approximation by interpolation of the state

- **Approximation** of the state $\phi(\gamma, t)$, for $\{\gamma_p\}_{0 \leq p \leq P+1} \subset \mathcal{C}$
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- The corresponding **realization** reads :

$$\partial_t \phi_p(t) = \gamma_p \phi_p(t) + u(t), \quad 1 \leq p \leq P,$$

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- **Convergence results** can be proved, as $\dim. P \longrightarrow \infty$.

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- 2 Systems under consideration
 - Integral representations with poles and cuts
 - Finite-dimensional approximation by interpolation
- 3 **Specialized optimization procedures**
 - Functional spaces and measures
 - Regularized criterion with equality constraints
 - Numerical optimization
- 4 Applications
 - Fractional systems
 - Irrational systems
- 5 Conclusion and Perspectives

Re-interpreting Sobolev spaces

- Optimization in the **frequency** domain, stemming from

$$\widehat{h}(f) = \lim_{\epsilon \rightarrow 0^+} H(\epsilon + 2i\pi f)$$

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- Norms in L^2 , or Sobolev spaces H^s , are defined as :

$$\|h\|_{H^s(\mathbb{R}_t)}^2 = \int_{\mathbb{R}_f} w_s(f) |H(2i\pi f)|^2 df, \text{ with } w_s(f) = (1 + 4\pi^2 f^2)^s.$$

where $s \in \mathbb{R}$ tunes the balance between low and high frequencies.

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- For specific applications, more general **frequency dependent weights** can be used : bounded frequency range, logarithmic scale, relative error measurement, bounded dynamics ...

Building up specific weights for audio applications

For audio applications, $w(f)$ can be adapted and modified according to the following requirements :

- 1 a **bounded frequency** range $f \in [f^-, f^+] : w(f) 1_{[f^-, f^+]}(f)$;

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- 3 a **relative error** measurement : $w(f)/|H(2i\pi f)|^2$
- 4 a relative error on a **bounded dynamics** :
 $w(f)/(\text{Sat}_{H,\Theta}(f))^2$ where the saturation function $\text{Sat}_{H,\Theta}$ with **threshold** Θ is defined by

$$\text{Sat}_{H,\Theta}(f) = \begin{cases} |H(2i\pi f)| & \text{if } |H(2i\pi f)| \geq \Theta_H \\ \Theta_H & \text{otherwise} \end{cases}$$

Note : normalization of the samples is desirable in most audio applications, before the sequence is sent to DAC audio converters.

Regularized criterion with equality constraints

- The regularized criterion reads :

$$C_R(\mu) = \int_{\mathbb{R}^+} \left| \widetilde{H}_\mu(2i\pi f) - H(2i\pi f) \right|^2 w(f) df + \sum_{p=1}^P \epsilon_p |\mu_p|^2,$$

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- Equality constraints for $\widetilde{H}_\mu^{(d_j)}$ at **prescribed frequency** points η_j , $1 \leq j \leq J$ are taken into account thanks to a Lagrangian $\mathcal{C}_{R,L}$ by adding to \mathcal{C}_R :

$$\Re \left(\ell^* \begin{bmatrix} H^{(d_1)}(2i\pi\eta_1) - \widetilde{H}_\mu^{(d_1)}(2i\pi\eta_1) \\ \vdots \\ H^{(d_J)}(2i\pi\eta_J) - \widetilde{H}_\mu^{(d_J)}(2i\pi\eta_J) \end{bmatrix} \right),$$

Discrete criterion

- Discrete version of the criterion for frequencies increasing from $f_1 = f_-$ to $f_{N+1} = f_+$ is, with $s_n = 2i\pi f_n$:

$$\mathcal{C}(\mu) \approx \sum_{n=1}^N w_n \left| \widetilde{H}_\mu(s_n) - H(s_n) \right|^2 \quad \text{with } w_n = \int_{f_n}^{f_{n+1}} w(f) df.$$

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- In matrix notations, this rewrites

$$\mathcal{C}_{R,L}(\mu) = (\mathbf{M}\mu - \mathbf{h})^* \mathbf{W}(\mathbf{M}\mu - \mathbf{h}) + \mu^t \mathbf{E}\mu + \Re(\ell^* [\mathbf{k} - \mathbf{N}\mu]),$$

$$\text{with } \left\{ \begin{array}{ll} \mathbf{M} : & \text{model} \quad N \times (P + P_2) \\ \mathbf{N} : & \text{constraint model} \quad J \times (P + P_2) \\ \mathbf{E} : & \text{regularization} \quad (P + P_2) \times (P + P_2) \\ \mathbf{W} : & \text{weights} \quad N \times N \\ \mathbf{h} : & \text{data} \quad N \times 1 \\ \mathbf{k} : & \text{constaints} \quad J \times 1 \end{array} \right.$$

Closed-form solution

- If $J = 0$ (no constraint), the solution reduces to

$$\boldsymbol{\mu} = \mathcal{M}^{-1} \mathcal{H},$$

where $\mathcal{M} = \Re\left(\mathbf{M}^* \mathbf{W} \mathbf{M} + \mathbf{E}\right)$ and $\mathcal{H} = \Re\left(\mathbf{M}^* \mathbf{W} \mathbf{h}\right)$.

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- For $\mathbf{J} \geq 1$, the solution reads :

$$\boldsymbol{\mu} = \mathcal{M}^{-1} \left[\mathcal{H} + \underline{\mathbf{N}}^t \mathcal{N}^{-1} \left(\underline{\mathbf{k}} - \underline{\mathbf{N}} \mathcal{M}^{-1} \mathcal{H} \right) \right],$$

where $\mathcal{N} = \underline{\mathbf{N}} \mathcal{M}^{-1} \underline{\mathbf{N}}^t$ is invertible for non-redundant constraints, and

$$\begin{cases} \underline{\mathbf{N}}^t & \text{denotes } [\Re(\underline{\mathbf{N}}^t), \Im(\underline{\mathbf{N}}^t)] \\ \underline{\mathbf{k}}^t & \text{denotes } [\Re(\underline{\mathbf{k}}^t), \Im(\underline{\mathbf{k}}^t)] \end{cases} .$$

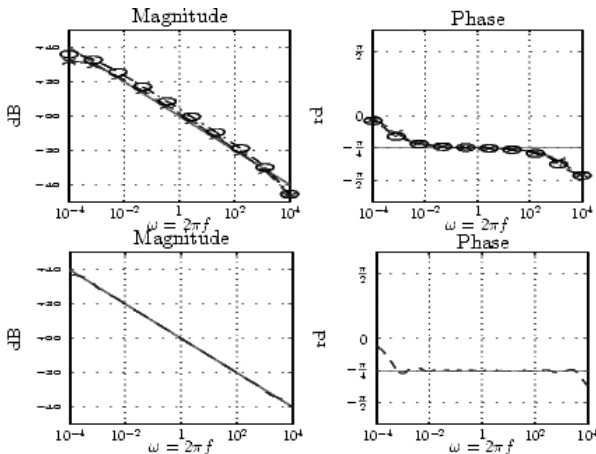
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Fractional systems

An academic example :

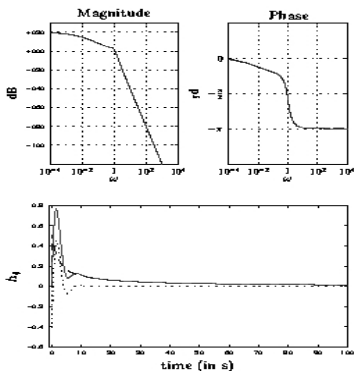
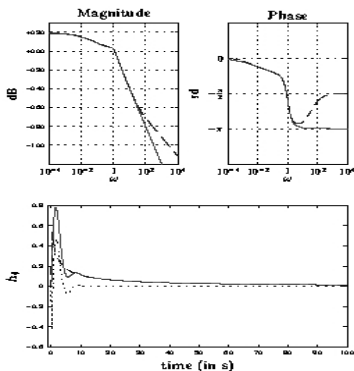
$$H_1(s) = 1/\sqrt{s}, \mu_1(-\xi) = 1/(\pi\sqrt{\xi})$$



Top : Interpolation, $P = 16$. Bottom : Optimization, $P = 10$!

Fractional systems

Fractional AR : $H_3(s) = 1/(s^2 + 0.1s^{3/2} + s^{1/2} + 0.1)$
 (poles and \mathbb{R}^-)

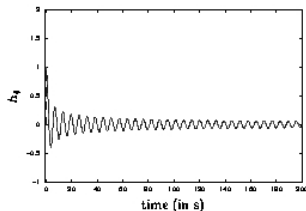
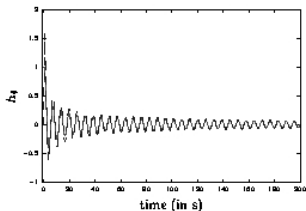
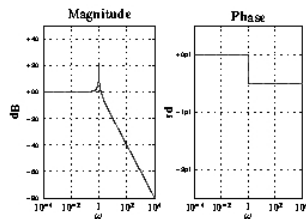
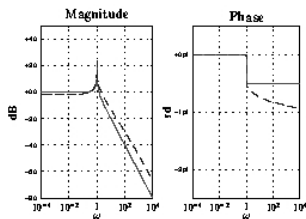


Left : Interpolation, $P = 18$. **Right** : Optimization, $P = 18$!
 (\dots) : poles only. $(- -)$: cut only. $(-)$: poles and cut.

Irrational systems

Bessel kernel : 2 cuts $\pm i + \mathbb{R}^-$

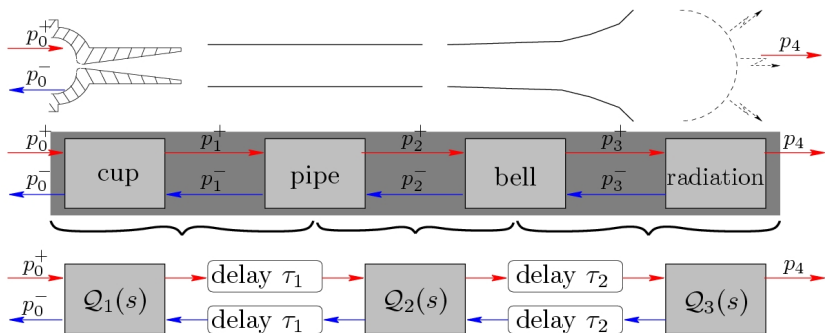
$$H_4(s) = 1/\sqrt{s^2 + 1}, \quad \mu_4^\pm(-\xi) = 1 / (\pi\sqrt{\xi(\pm 2i - \xi)})$$



Left : Interpolation, $P = 10$. Right : Optimization, $P = 10!$

Trumpet-like instrument (I)

Decomposition into elementary subsystems.



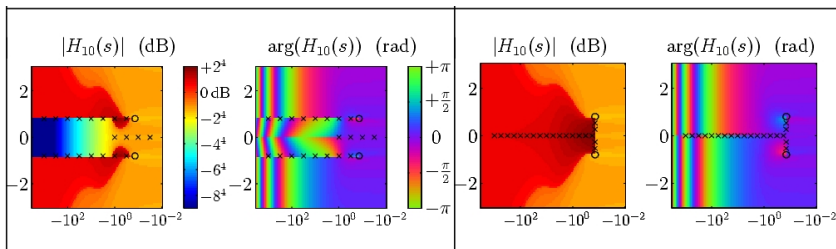
Transfer functions of interest :

- **Reflection** between p_0^+ and p_0^- .
- **Transmission** between p_0^+ and p_4 .

Trumpet-like instrument (II) : various choices of the cuts

- with 3 **Horizontal** cuts,

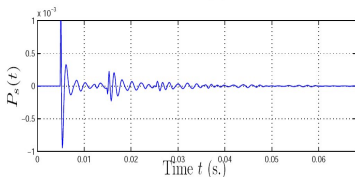
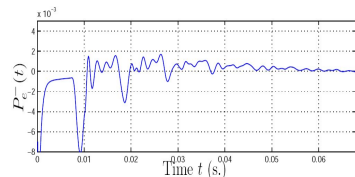
- with a **Cross** cut



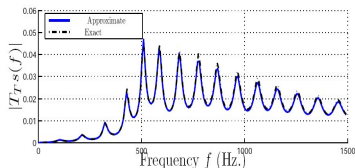
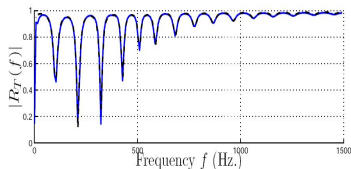
- Remark** : the values of $H(s)$ in \mathbb{C}_0^+ do **not** depend on the choice of the cut!

Trumpet-like instrument (III)

Time-domain representation



Frequency-domain rep.



Real-time simulations in Pure-Data environment on optimized models with $P \leq 10$ for each quadripole Q_k : bounded freq. range, log-scale & relat. error.

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Perspectives

- Open question : choice of the cut ?

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- Open question : optimal placement of the poles, once the cut has been chosen ?

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- Open question : choice of the cut ?
- Open question : optimal placement of the poles, once the cut has been chosen ?
- What can *not* be represented by poles and cuts ?
 - *Delay* systems stemming from *wave propagation* phenomena.
 - systems of PDEs with *variable* coefficients : must be decomposed into subsystems with constant coefficients.

Conclusion

- A powerful and very flexible method of simulation of some *infinite*-dimensional linear systems has been presented : it uses a simple **optimization** procedure with parameters which are meaningful from a **signal processing** point of view, and it enables a **low cost** simulation (both in the frequency domain and in the time domain), even suitable for **real-time** applications.

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- From a theoretical point of view, this method is based on a *representation with poles and cuts*, which generalizes the so-called **diffusive representations**.
- Many such systems, among which **fractional differential systems**, have been presented here and elsewhere, which clearly illustrates the generality, the flexibility and the power of this method.

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